

Timber Frame Wall Tie

FT-75

Tested Values

	Compression (kN)	Y _m	Tension (kN)	Y _m
Nail end (as received)	0.504		0.672 (nail withdrawal)	1.3 ⁽¹⁾
(24mm movement)	0.582	1.15 ⁽³⁾ (buckling of tie – steel failure)	0.690	
Masonry end	0.786	1.15 ⁽³⁾ (buckling of tie – steel failure)	2.265 (masonry withdrawal)	3 ⁽²⁾

- (1) from BS EN1995-1-1 table 2.3 connections (fixing withdrawal of tie)
- (2) from NA to BS EN1996-1-1 table NA.1 (mortar failure of tie)
- (3) from NA to BS EN1995-1-1 table NA.3 (steel buckling of tie)

Based on the following criteria the following calculations have been done:

In the following examples a factored windload of 1.65kN/m² is suggested

Partial factor for variable action		1.5
Combined pressure coefficient		1.1
Peak velocity pressure		= 1.0 kN/m ²
Applied wind load on gable panel	= 1.5 x 1.1 x 1.0	= 1.65 kN/m ²

Failure	Test Result (kN)	Y _m	kmod	Result x kmod / Y _m (kN)
Compression	0.504	1.15	1.1	0.482
Tension	0.672	1.3	1.1	0.568
Tension	2.265	3	1.1	0.830
Compression	0.786	1.15	1.1	0.751
				0.482

^{*}An instantaneous action (kmod value - 1.1) has been used.

Maximum net surface wind pressure for the FT-75

Parket Oct	Vertical Tie Spacing (mm)							
	22	5	30	0	37	5	450)
	Stud Centres (mm)							
Product Code	60	0	60	0	60	0	600)
	Maximum Net Surface Wind Pressure							
	kN/m²	ties/m²	kN/m²	ties/m²	kN/m²	ties/m²	kN/m²	ties/m²
FT-75	3.56	7.4	2.65	5.5	2.12	4.4	1.78	3.7

	1000/225 = 4.4444 4.4444x(1000/600) = 7.4 ties/m ²	1000/300 = 3.3333 3.3333x(1000/600) = 5.5 ties/m ²	1000/375 = 2.6666 2.6666x(1000/600) = 4.4 ties/m ²	1000/450 = 2.2222 2.2222x(1000/600) = 3.7ties/m ²	
Lowest failure (with Ym & kmod applied)	0.482 x 7.4 = 3.56kN/m ²	0.482 x 5.5 = 2.65kN/m ²	0.482 x 4.4 = 2.12kN/m ²	0.482 x 3.7 = 1.78kN/m ²	
Peak velocity pressure (kN/m²)	2.157	1.606	1.284	1.078	

Based on the above values this could be worked backwards
Provide a maximum wind load for 3.7 ties/m2 = (1.78/1.1/1.5) = 1.078kN/m2 peak velocity pressure